

# **DuPont™ Cyclotene™**

Advanced Electronics Resins

Adhesion of Cyclotene™ Advanced Electronics Resins

# **Regional Product Availability**

- North America
- Europe, Middle East and Africa
- Latin America
- Asia-Pacific

## Introduction

In fabricating a semiconductor device or package, adhesion of the materials used to one another is one of the most important considerations. Typically, multiple layers of polymers, metals, and inorganic glasses are used, and these layers must adhere well to each other to survive reliability testing. The adhesion of Cyclotene™ Advanced Electronics Resin,\* derived from B-staged bisbenzocyclobutene (BCB) monomers, to various materials is thus of vital importance in fabricating a reliable device.

This application note discusses the various aspects of Cyclotene™ Resin adhesion. Section 2 describes the chemistry of the two adhesion promoters offered by DuPont. Section 3 reviews processing procedures, and section 4 briefly summarizes the interfacial science involved. Section 5 covers pre-clean procedures, which are crucial in obtaining reliable adhesion. Section 6 describes the effects of processing chemicals, and section 7 reviews the adhesion test methods used to generate the data that is reported here. In sections 8–10 we review the adhesion of Cyclotene™ Resin deposited on top of other materials, while in sections 11–13 the adhesion of other materials on top of Cyclotene™ Resin is discussed.

## **Adhesion Promoter Chemistry**

Two adhesion promoter solutions are available from DuPont, AP8000 and AP3000. Both are based on organosilane primer chemistry.

These adhesion promoters are supplied as dilute solutions of the organosilane compounds in 1-methoxy-2-propanol. They are ready to use, and dilution or mixing may result in reduced adhesion. **Table 1** shows the composition and sales specs of the two products.

During the manufacture of AP3000 and AP8000, the silanes are hydrolyzed by a proprietary process. This converts some of the alkoxysilane or acetoxysilane groups to silanols (Si-OH), which

partially condense to form siloxane oligomers. It is the silane oligomers containing silanol groups that are believed to be the active components in the adhesion promoter solutions.

AP3000 and AP8000 are the only adhesion promoters recommended for use with Cyclotene $^{\text{\tiny M}}$  Resins. In particular, hexamethyldisilazane (HMDS) is not effective as a Cyclotene $^{\text{\tiny M}}$  resin adhesion promoter.

## **Adhesion Promoter Application**

To prepare the surface for Cyclotene™ Resin coating, the adhesion promoter solution is applied to the surface of the substrate, which is then spun dry. The substrate surface is immediately ready for BCB coating. AP3000 and AP8000 are designed for spin coating, and vapor priming of these is not recommended. The adhesion promoters improve the adhesion of BCB to most surfaces, and their use is virtually always recommended.

The basic function of an adhesion promoter is to form a compatible interface between two otherwise incompatible materials. The mechanism of adhesion derives from condensation of silanols with surface oxygen atoms or hydroxyl groups. The surface of the metal or inorganic material is then covered with an organosilane, with the organic portion facing outward. This renders the surface more compatible with an organic polymer.

AP3000 often provides better adhesion than AP8000. The presence of the vinyl group in AP3000, which can react with the benzocyclobutene groups in the resin, is sometimes cited as a reason for this improvement. However, concrete data to support this is lacking. On some surfaces, AP8000 works quite well, despite its lack of apparent functional groups that can react with the BCB polymer. The actual mechanism of interaction between BCB and the adhesion promoter remains unclear. **Table 2** shows adhesion to silicon as a function of time delay between AP3000 coat and bake, and Cyclotene™ Resin coat and bake. The adhesion does not degrade significantly even after a 7 day delay. Note that data is available only for cases where the AP3000-treated surface has been baked.

# The Nature of the Adhesion Promoter Layer

The coating of adhesion promoter on the substrate is quite thin. Figure 1 shows thickness of an AP3000 layer (measured by ellipsometry) versus spin speed and bake temperature. Figure 2 shows that after a rinse with mesitylene (T1100) there is still a thin layer remaining. Though the thickness of the AP3000 layer is dependent on the coating spin speed, the adhesion is independent of the thickness.

The effectiveness of the adhesion promoter can often be enhanced by baking, and data on specific substrates will be shown below. The effect of a hot plate bake on the surface appearance of the coating, as measured by atomic force microscopy (AFM), is shown in **Figure 4**. Baking produces a more uniform coating.

**Table 1. Adhesion Promoter Composition and Sales Specs** 

	AP3000	AP8000
Silane	0.24-0.36%	0.096-0.144%
Particles	25 max*	25 max*
Sodium	1 ppm max	1 ppm max
Potassium	1 ppm max	1 ppm max
Copper	1 ppm max	1 ppm max
Iron	1 ppm max	1 ppm max
Nickel	1 ppm max	1 ppm max
Total Metals	10 ppm max	10 ppm max
Shelf Life	2 years	2 years

\*particles/mL, greater than or equal to 0.5  $\mu m$ 

Table 2. Effect Of Time Delay Between AP3000 Application (coat and bake) and Cyclotene™ Resin Coating on Adhesion to Silicon

			_		
Cyclotene™ 3022-57 Advanced Electronics Resin					
				Та	pe peel test
AP3000?	Bake?	Time delay	m-ELT (Kc)	Dry	After 48 hr PCT
Yes	Yes	0	0.33 ± 0.02	5B	5B
Yes	Yes	18 hr	$0.33 \pm 0.02$	5B	5B
Yes	Yes	24 hr	$0.32 \pm 0.02$	5B	5B
Yes	Yes	40 hr	$0.32 \pm 0.03$	5B	5B
Yes	Yes	166 hr	$0.30 \pm 0.03$	5B	5B
Cyclotene™ 4024-40					
				Ta	ne neel test

Cyclotene 4024-40					
			Та	pe peel test	
AP3000?	Bake?	Time delay	m-ELT (Kc)	Dry	After 48 hr PCT
Yes	Yes	0	$0.33 \pm 0.01$	5B	5B
Yes	Yes	18 hr	$0.33 \pm 0.03$	5B	5B
Yes	Yes	24 hr	$0.32 \pm 0.03$	5B	5B
Yes	Yes	40 hr	$0.32 \pm 0.03$	5B	5B
Yes	Yes	166 hr	$0.30 \pm 0.03$	5B	5B

## **Substrate Pre-Clean**

A clean surface, free of particles and organic contaminants, is important to achieve a robust interface between Cyclotene™ films and the underlying substrate. Several different pre-clean procedures have been used, depending on available equipment. Some examples are:

- O<sub>2</sub> plasma
- O<sub>2</sub> plasma; water rinse
- O<sub>2</sub>/CF<sub>4</sub> plasma; water rinse
- O<sub>2</sub>/CF<sub>4</sub> plasma; acetic acid rinse; water rinse
- Ar plasma; water rinse
- Resist stripper; water rinse
- O<sub>2</sub> plasma; resist stripper; water rinse

Each of these can be used successfully, but problems can arise if not done correctly. With some types of plasma tools, an  $O_2/CF_4$  plasma can create oxyfluorides on the metal surface which can degrade adhesion. Aluminum seems particularly prone to this. Resist strippers have been used but adhesion problems can arise from residues due to incomplete rinsing. The most generally applicable pre-clean procedure is an  $O_2$  plasma, with or without water rinse. RIE (reactive ion etch) type plasma tools appear to give the best results, and are preferred over barrel etchers and microwave plasma tools.

An example of the effect of plasma cleaning treatments is shown in **Table 3**. In this case,  $O_2/CF_4$  plasma made adhesion worse relative to the control. Bump shear was used to measure these adhesion values (see section 6 below).

Figure 1. AP3000 Thickness vs. Spin Speed and Bake Temperature

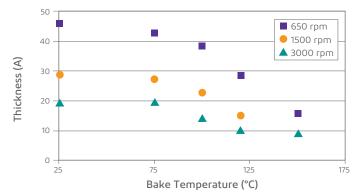


Figure 2. AP3000 Thickness Before and After Rinse with Mesitylene (t1100)

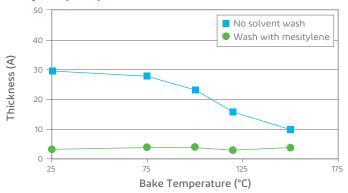
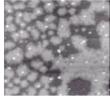


Figure 3. AP3000 Coating Uniformity vs. Bake Temperature (AFM)







No Bake

100 °C Bake

180 °C Bake

# **Effect of Processing Chemical**

Some etch chemicals can attack the interface and cause undercut or delamination of Cyclotene™ films from the underlying surface. Sometimes this is not an attack of the adhesion promoter but rather etching of the substrate; delamination occurs because the cured BCB film is under tensile stress, causing the etchant to continue to attack the interface. The chemical sensitivity is substrate-dependent, as is shown in Table 4. In general, chemicals that can etch the material under the BCB can cause undercut or delamination.

Dilute solutions of HF, or buffered oxide etch (BOE) can be used with BCB films but higher concentrations should be avoided. For example we found that BCB on silicon nitride would tolerate 3 minutes in 2% HF, whereas in 11% HF the etch time could not be more than 10 seconds.

## **Adhesion Test Methods**

A number of different methods have been used to measure the adhesion of thin films. This report uses data obtained from three different test methods: tape peel, modified edge lift-off (m-ELT), and bump shear. The tape peel test is based on ASTM D-3359-93. In this test, the film is scratched with a set of parallel blades to form a 10 x 10 grid of 1 mm squares. The rating is a semi-quantitative description of the damage after attachment and removal of the tape. Ratings range from OB (large portions of the film delaminated) to 5B (no film loss or film damage). Films are tested dry (no temperature/humidity stressing) and after a pressure cooker test (PCT). The conditions in the PCT are: 121 °C, 2 atmospheres pressure, 100% relative humidity.

m-ELT is a fracture mechanics-based approach to adhesion measurement. A thick layer of epoxy is applied on top of the device to be tested. The structure is cleaved to expose an edge, and the temperature of the device is lowered until the stress in the system causes the applied energy to exceed the fracture energy. The structure will fail either adhesively (peeling), or cohesively (fracture inside one of the layers). Interfacial energy (Kc, in units of MPa·m<sup>0.5</sup>) is calculated based on the temperature at which the structure fails. This test has been described in more detail elsewhere (1).

In the bump shear test, squares of Cyclotene $^{\times}$  film (typically 100  $\mu$ m x 100  $\mu$ m) are patterned on the substrate and are sheared off with a bump shear tool. The adhesion value reported is the force required to shear or fracture the bump. This test method has been described by Toepper et. al. (2)

Table 3. Cyclotene™ Film Adhesion to Aluminum with Different Plasma Pre-Clean Procedures

Pre-Clean Procedure	Bump Shear Force (g)	
Control (water rinse)	49.1 ± 2.6	
O <sub>2</sub> /CF <sub>4</sub> plasma	42.5 ± 3.5	
O <sub>2</sub> plasma	$60.7 \pm 3.7$	

Table 4. Sensitivity of Cyclotene™ Film Interfaces to Etch Chemicals

Interface	Etch Chemical	Result
BCB on SiO <sub>2</sub>	HF	Delamination
BCB on SiO <sub>2</sub>	HCl or H <sub>2</sub> SO <sub>4</sub>	No delamination
BCB on Cu	HF	No delamination
BCB on Cu	HCl or H <sub>2</sub> SO <sub>4</sub>	Delamination

# **BCB** on Top of Metals

#### **Aluminum**

While excellent adhesion to aluminum is usually seen, this surface is especially sensitive to surface contamination, and the pre-clean procedure is very important (see section 5 and **Table** 3). If using an O₂/CF₄ pre-clean procedure, care must be taken to ensure that the aluminum surface is not converted to a high proportion of aluminum oxyfluoride, which may degrade the adhesion. Note that if you are integrating more than one layer of photosensitive Cyclotene™ film with aluminum, the first layer will require a descum step with a fluorinated plasma, and this step must also leave an undamaged aluminum surface for the next layer of Cyclotene™ film.

Adhesion to aluminum can be improved by baking the adhesion promoter. **Figure 4** shows adhesion of Cyclotene™ 4024-40 Advanced Electronics Resin to aluminum vs. AP3000 bake temperature. In general, K1c values above 0.30 are associated with good adhesion and reliability.

AP8000 is not effective as an adhesion promoter for BCB on aluminum, and the use of AP8000 with aluminum is not recommended.

Table 5 shows adhesion of photosensitive Cyclotene™ film to various substrates, including aluminum, with and without AP3000 and with and without AP3000 bake. Adhesion is clearly enhanced by the adhesion promoter bake. These adhesion measurements were by tape peel test.

#### Copper

**Figure 5** shows adhesion of Cyclotene<sup>™</sup> 4024-40 to copper vs. bake temperature. There is an improvement in adhesion when the bake is applied.

Issues have occasionally been seen with adhesion of BCB to the side wall of high aspect ratio copper lines. This is believed to be related to the difficulty of cleaning these narrow trenches. RIE may be relatively ineffective, especially if the side wall slope is retrograde.

**Table 5** shows tape peel adhesion data for photo sensitive Cyclotene<sup>™</sup> film on copper, with and without AP3000, and with and without an AP3000 bake.

#### **Titanium**

**Table 6** shows adhesion data for Cyclotene™ 4022-35 to titanium. Adhesion of BCB to Ti is poor without adhesion promoter but is quite good when AP3000 is used, particularly when the AP3000 is baked.

#### Gold

Cyclotene™ film does not adhere well to gold, or to other noble metals. BCB has been successfully used to completely cover gold lines and features, but if an opening in the film lands on gold, loss of adhesion may occur. The most likely explanation is that since gold does not form a surface oxide, there are no oxygen atoms on the surface for the silane to bond with. It is recommended that the BCB on gold interface be avoided if at all possible, and an intermediate layer (e.g., silicon nitride) be used to provide a surface for BCB adhesion.

Figure 4. Adhesion of Cyclotene™ 4024-40 Advanced Electronics Resin to Aluminum, With and Without a 60 Second AP3000 Bake (m-ELT data)

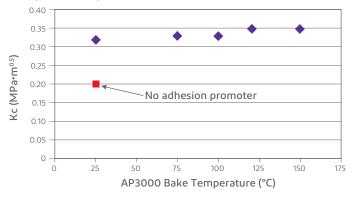
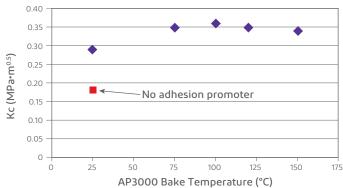


Table 5. Adhesion of Photosensitive Cyclotene™ Films to Various Substrates by Tape Peel Test, After a 96 Hour Pressure Cooker Test

Substrate	No AP3000	AP3000, No Bake	AP3000, Bake ≥75°C
Aluminum	0B	3B	5B
Copper	0B	4B	5B
SiO <sub>2</sub>	0B	5B	5B
SiNx	5B	5B	5B

Figure 5. Adhesion of Cyclotene™ 4024-40 Advanced Electronics Resin to Copper, With and Without a 60 Second AP3000 Bake (m-ELT data)



# **BCB** on Top of Inorganic Materials

## Silicon Nitride

**Figure 6** shows the adhesion of Cyclotene<sup>™</sup> 4024-40 Advanced Electronics Resin to silicon nitride as a function of AP3000 bake temperature. **Table 5** shows data for Cyclotene<sup>™</sup> film adhesion to nitride, with and without AP3000 and with and without a bake.

## Silicon Oxide

**Figure 7** shows the adhesion of Cyclotene™ 4024-40 to silicon oxide versus AP3000 bake temperature. **Table 5** shows data for Cyclotene™ film adhesion to oxide, with and without AP3000 and with and without a bake.

R. Dauskardt et. al. have studied the sub-critical debonding of Cyclotene™ 3022 to silicon oxide using double cantilever beam and 4-point bend test structures (3,4). While both adhesion promoters greatly improved the adhesion of BCB to oxide, they found slightly better adhesion with AP3000 than with AP8000.

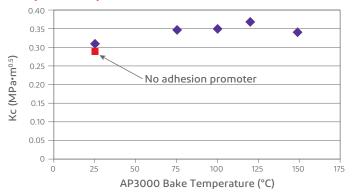
#### **III-V Semiconductors**

Cyclotene™ film adhesion to III-V semiconductors (GaAs, InP) tends to be marginal, even with the use of AP3000. As with gold, it is best to avoid this interface and employ an intermediate layer (e.g., silicon nitride or Ti) to which BCB has good adhesion once an adhesion promoter is applied.

Table 6. Adhesion of Cyclotene™ 4022-35 Advanced Electronics Resin to Ti by Tape Peel Test

Surface	m-ELT	Dry	Tape Peel 48 hr PCT
No AP3000	0.14 ± 0.04	0B	0B
AP3000, no bake	$0.31 \pm 0.02$	5B	4B
AP3000, baked	0.35 ± 0.02	5B	5B

Figure 6. Adhesion of Cyclotene™ 4024-40 Advanced Electronics Resin to Silicon Nitride, With and Without a 60 Second AP3000 Bake (m-ELT data).



# **BCB** on Top of Organic Polymers

## **BCB** to BCB

Cure management is important when stacking multiple layers of Cyclotene™ Resin. For the top layer of BCB to properly stick to the layer below it, the bottom layer must be partially cured (75–85%). Figure 7 shows BCB-BCB adhesion as a function of the cure temperature of BCB1 (2). At low cure temperatures (% cure = 77–85%) the adhesion is excellent; as the cure level increases the polymer-polymer adhesion degrades rapidly.

Because there is some silicon in the BCB polymer backbone, an oxidizing plasma process (e.g.,  $O_2$  plasma) can leave a thin layer of  $SiO_2$  on the BCB surface. This layer has poor mechanical properties, and will adversely affect the adhesion of BCB (or anything else) deposited on top. Descum or plasma etch recipes must be optimized such that the silicon etch is balanced with the organic polymer etch, and silicon does not accumulate on the surface.

Several different pre-clean procedures have been used, depending on available equipment. Some examples are:

- O<sub>2</sub>/CF<sub>4</sub> plasma; water rinse
- O<sub>2</sub>/CF<sub>4</sub> plasma; acetic acid rinse; water rinse
- Ar plasma; water rinse
- Resist stripper; water rinse

Each of these can be used successfully, but problems can arise if not done correctly. With some types of plasma tools, an  $O_2/CF_4$  plasma can create oxyfluorides on the metal surface which can degrade adhesion. Aluminum seems particularly prone to this. Resist strippers have been used but adhesion problems can arise from residues due to incomplete rinsing. The most generally applicable pre-clean procedure is an  $O_2$  plasma, with or without water rinse. RIE (reactive ion etch) type plasma tools appear to give the best results, and are preferred over barrel etchers and microwave plasma tools.

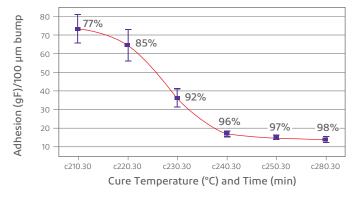
Adhesion promoter appears to have little effect on BCB-BCB adhesion. Normally, in a multilayer construction, the BCB will contact metals or other materials in addition to the underlying BCB layer and the adhesion promoter is highly recommended. In the unusual circumstance where BCB is deposited over a blanket film of BCB, adhesion promoter is not required.

# **BCB** to Polyimide

We have studied the adhesion of Cyclotene $^{\text{TM}}$  4024-40 Advanced Electronics Resin to polyimide. The polyimide was subjected to a dehydration bake at 150 °C and an  $O_2$  plasma treatment prior to Cyclotene $^{\text{TM}}$  Resin coating. The BCB layer was fully cured. Tape peel tests gave 5B ratings (excellent adhesion) immediately after cure as well as after a 48 hour pressure cooker test. Adhesion of BCB to polyimide appears to be strong. We believe the oven bake and  $O_2$  plasma treatment are important in obtaining good adhesion between the polymers.

Note that there are several manufacturers of polyimides, and many different grades. We have not tested them all and cannot guarantee the same quality of adhesion to all polyimide types.

Figure 7. BCB-BCB Adhesion vs. BCB1 Cure Temperature, Measured by Bump Shear Test (the degree of cure of each point is indicated on the graph)



# Metals on Top of BCB

## **Sputtering**

The most important consideration in ensuring good adhesion of a sputtered metal film to Cyclotene™ Resin is that a sputter etch is required. The sputter etch, typically argon, should be done in situ without breaking vacuum. A 100 Å equivalent silicon oxide etch is very common and gives reliably good adhesion.

Cyclotene™ film surface damage by an oxidizing plasma can weaken the bond between metal and BCB significantly (see section 9.1). Minor surface oxidation might be repaired by the sputter etch, but significant surface oxidation will likely result in decreased adhesion.

Aluminum can be sputtered on top of BCB directly; no intermediate layers are needed. Copper generally does not adhere well when sputtered directly on BCB, so another layer is needed here. The adhesion layer is typically a thin layer of Ti or Ti:W. Shieu and Shiao (6) found poor adhesion of copper when either the argon ion pre-treatment or a Ti adhesion layer was omitted, whereas when both of these were employed the adhesion was quite strong. Evidence of direct bonding between BCB and Ti was seen in the form of Ti-C bonds at the BCB-metal interface.

Gutmann et. al. found that a Cu-C film (1–2% C) improved the adhesion of copper to BCB (7). They also found that the adhesion was better after damascene processing of the BCB, which they attributed to increased surface roughness and chemical modification of the BCB surface due to plasma etching.

Chromium can be sputtered onto BCB, and adheres well. Sputtered chromium, however can be highly stressed, and metal cracking can occur unless sputtering conditions are carefully controlled. It is generally preferred to use Ti or Ti:W instead of Cr.

# **Evaporation**

In general, the metals that can be sputtered can also be evaporated. The need for an in situ sputter etch still holds, however. This means that the metal evaporation system should be equipped with an argon ion gun or ion mill. **Table 7** lists the adhesion of Ti, Cu, and Cr under different deposition methods.

Cyclotene™ film surface damage by an oxidizing plasma can weaken the bond between metal and BCB significantly (see section 9.1). Minor surface oxidation might be repaired by the ion milling treatment, but significant surface oxidation will likely result in decreased adhesion.

# Inorganic on Top of BCB

#### Silicon Nitride

Integration of PECVD silicon nitride on top of Cyclotene™ Resin has been implemented in production by several customers.

It is important to remain within the thermal budget of BCB, otherwise thermal degradation of the polymer may result. The deposition temperature should be no higher than 350 °C, preferably lower.

The adhesion of nitride to BCB tends to be better when  $N_2$  rather than  $NH_3$  is the nitrogen source.  $NH_3$  plasma can damage the BCB surface. If  $SiH_4/NH_3$  chemistry is used, the  $NH_3$  predeposition time should be as short as possible; preferably,  $N_2$  should be introduced to the chamber first, then  $NH_3$  as the plasma stabilizes.

#### Silicon Oxide

A study of the adhesion of PECVD silicon oxide ( $SiH_4 + N_2O$ ) to dry etch Cyclotene<sup>TH</sup> Resin found that a nitrogen plasma pre-treatment greatly improved the adhesion of the oxide (8). Pretreatment with  $NH_3$  or  $N_2O$  plasma, by contrast, yielded no improvement at all in adhesion. As with silicon nitride deposition, it is important to stay below the thermal decomposition temperature of BCB (about 350 °C).

Table 7. Adhesion of Metals to BCB vs. Pre-Deposition Surface Treatment

Metal	Deposition	Pre-Treatment	Tape Peel Result
Ti	Sputter	None	0B
Ti	Sputter	Ar sputter etch	4B
Ti	Evaporate	Ar ion gun	4-5B
Cr	Sputter	None	3B
Cr	Sputter	Ar sputter etch	4B
Cr	Evaporate	Ar ion gun	4B
Cu	Sputter	None	0B
Cu	Sputter	Ar sputter etch	0B
Cu	Evaporate	None	0B
Cu	Evaporate	Ar ion gun	2B

# Organic Polymers on Top of BCB

## Underfill

Underfills, typically silica-filled epoxy resins, are used in flip chip applications. Researchers at Georgia Tech (9) studied the adhesion of several commercially available underfill materials to Cyclotene™ Resin by die shear testing. They found generally very good adhesion. Failure analysis of the sheared parts revealed mixed mode failures, with adhesive failure at the BCB/SiO<sub>2</sub> or BCB/nitride interface, adhesive failure at the BCB/underfill interface, and cohesive failure of the underfill all present.

Dimke and Edwards (10) studied adhesion of underfills to several difference passivation materials. They saw a large variation in the results depending on the choice of underfill, and the optimum choice was dependent on the type of passivation material. There are many commercially available underfill formulations, and it is important to work with the underfill supplier to select the product most compatible with BCB.

Researchers at Stanford University also studied BCB adhesion to commercial underfill resins (11). Failure occurred predominantly at BCB-nitride, not at the BCB-underfill interface. Despite this, the adhesion values varied considerably depending on which underfill was used, again highlighting the importance of underfill selection. They found the adhesion values to be higher with partially cured BCB than with fully cured BCB.

## **Molding Compound**

Molding compounds, like underfills, are filled epoxy resins. Problems with this interface are unusual. We have seen that the adhesion of molding compound to partially cured BCB is stronger than to fully cured BCB. A UV-ozone treatment of the BCB surface improves the adhesion. **Table 8** provides data on these parameters. The test is similar to a m-ELT test; the thickness of the molding compound is varied and the device is inspected for failure at 196 °C. A thicker molding compound layer without failure indicates better adhesion.

Table 8. Adhesion of Cyclotene™ 4026-46 Advanced Electronics Resin to Epoxy Molding Compound. Failure was Only Seen with Full Cure and no UV-Ozone Treatment.

Mold cmpd Thickness	BCB cure	UV-ozone	Failure at -196°C?
178 µm	98%	No	No
184 µm	98%	No	Yes
199 µm	98%	No	Yes
199 µm	98%	Yes	No
199 µm	82%	No	No
231 µm	82%	No	No
248 µm	82%	Yes	No
318 µm	98%	Yes	No

#### References

- J.-H. Im, E.O. Shaffer II, T. Stokich Jr., A. Strandjord, J. Hetzner, J. Curphy, C. Karas, G. Meyers, D. Hawn, A. Chakrabarti, S. Froelicher, "On the Mechanical Reliability of Photo-BCB-Based Thin Film Dielectric Polymer for Electronic Applications", Trans. ASME, 122, 28-33 (2000).
- M. Toepper, A. Achen, H. Reichl, "Interfacial Adhesion Analysis of BCB/TiW/Cu/PbSn Technology in Waferlevel Packaging", 2003 Electronic Components and Technology Conference, New Orleans, LA, p. 1843-1846.
- 3. J.M. Snodgrass, D. Pantelidis, M.L. Jenkins, J.C. Bravman, R.H. Dauskardt, "Subcritical debonding of polymer/silica interfaces under monotonic and cyclic loading", Acta Materialia, 50, 2395-2411 (2002).
- M. Jenkins, J. Snodgrass, A. Chesterman, R.H. Dauskardt, J.C. Bravman, "Atomic Force Microscopy Studies of Fracture Surfaces From Oxide/Polymer Interfaces", Mat. Res. Soc. Symp. Proc., 654, AA2.71 (2001).
- 5. Data provided by Michael Toepper, Fraunhofer-IZM.
- F.S. Shieu, M.H. Shiao, "Effect of a Ti Inter-layer on the bond strength and thermal stability of the Cu/benzocyclobutenedivinyl-tetramethyldisiloxane interface", J. Adhesion Sci. Technol., 12(1), 19-28 (1998).
- J.M. Neirynck, R.J. Gutmann, S.P. Murarka, "Copper/ Benzocyclobutene Interconnects for Sub-100 nm Integrated Circuit Technology: Elimination of High-Resistivity Metallic Liners and High-Dielectric Constant Polish Stops", J. Electrochemical Society, 146(4), 1602-1607 (1999).
- 8. E.O. Shaffer II, M.E. Mills, D.D. Hawn, J.C. Liu, J.P. Hummel, "A Method for Improving the Adhesion of PE-CVD SiO2 to Cyclotene™ 5021 Polymeric Interlayer Dielectric", Proceedings of IITC, San Francisco, CA, June 1998, p. 223-225.
- P. Garrou, D. Scheck, J.-H. Im, J. Hetzner, G. Meyers, D. Hawn, J. Wu, M.B. Vincent, C.P. Wong, "Underfill Adhesion to BCB (Cyclotene™) Bumping and Redistribution Dielectrics", IEEE Trans. on Advanced Packaging, 23(3), 568-573 (2000).
- 10. M. Dimke, M. Edwards, presentation given at IMAPS Flipchip Technology Workshop, Austin TX (2001).
- 11. R.J. Hohlfelder, D.A. Maidenberg, R.H. Dauskardt, "Adhesion of Epoxy Underfill to Benocyclobutene-Passivated Silicon", Journal of Materials Research (2000)

## **Handling Precautions**

Before using this product, associated generic chemicals or the analytical reagents required for its control, consult the supplier's Material Safety Data Sheet (MSDS)/Safety Data Sheet (SDS) for details on material hazards, recommended handling precautions and product storage.

**CAUTION!** Keep combustible and/or flammable products and their vapors away from heat, sparks, flames and other sources of ignition including static discharge. Processing or operating at temperatures near or above product flashpoint may pose a fire hazard. Use appropriate grounding and bonding techniques to manage static discharge hazards.

**CAUTION!** Failure to maintain proper volume level when using immersion heaters can expose tank and solution to excessive heat resulting in a possible combustion hazard, particularly when plastic tanks are used.

# Storage

Store products in tightly closed original containers at temperatures recommended on the product label.

# **Disposal Considerations**

Dispose in accordance with all local, state (provincial) and federal regulations. Empty containers may contain hazardous residues. This material and its container must be disposed in a safe and legal manner.

It is the user's responsibility to verify that treatment and disposal procedures comply with local, state (provincial) and federal regulations. Contact your DuPont Electronic Materials Technical Representative for more information.

## **Product Stewardship**

DuPont has a fundamental concern for all who make, distribute, and use its products, and for the environment in which we live. This concern is the basis for our product stewardship philosophy by which we assess the safety, health, and environmental information on our products and then take appropriate steps to protect employee and public health and our environment. The success of our product stewardship program rests with each and every individual involved with DuPont products—from the initial concept and research, to manufacture, use, sale, disposal, and recycle of each product.

## **Customer Notice**

DuPont strongly encourages its customers to review both their manufacturing processes and their applications of DuPont products from the standpoint of human health and environmental quality to ensure that DuPont products are not used in ways for which they are not intended or tested. DuPont personnel are available to answer your questions and to provide reasonable technical support. DuPont product literature, including safety data sheets, should be consulted prior to use of DuPont products. Current safety data sheets are available from DuPont.



electronics.dupont.com

# For more information on DuPont™ Cyclotene™ or other DuPont products, please visit our website.

The information provided in this data sheet corresponds to our knowledge on the subject at the date of its publication. It may be subject to revision as new knowledge and experience becomes available. This information is not intended to substitute for any testing you may need to conduct to determine for yourself the suitability of our products for your particular purposes. Since we cannot anticipate all variations in end-use and disposal conditions, DuPont makes no warranties and assumes no liability in connection with any use of this information. It is intended for use by persons having technical skill, at their own discretion and risk. Nothing in this publication is to be considered as a license to operate under or a recommendation to infringe any patent right.

CAUTION: Do not use in medical applications involving permanent implantation in the human body. For other medical applications, see "DuPont Medical Caution Statement," H-50102-5 and "DuPont Policy Regarding Medical Applications" H-50103-5.

DuPont", the DuPont Oval Logo, and all products, unless otherwise noted, denoted with TM, SM or ® are trademarks, service marks or registered trademarks of affiliates of DuPont de Nemours, Inc. © 2019 DuPont de Nemours, Inc. All rights reserved.

Form No. 888-00002, Rev 0 (06/19)